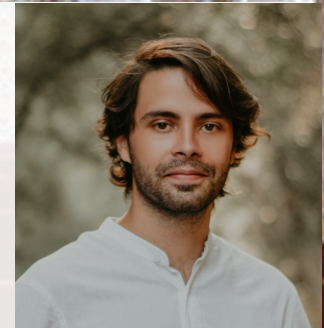


Fragility Function Uncertainty Quantification in Infilled RC Frame Buildings

Speaker: Al Mouayed Bellah Nafeh – IUSS Pavia

When: 12th June 2023

Where: Athens, Greece



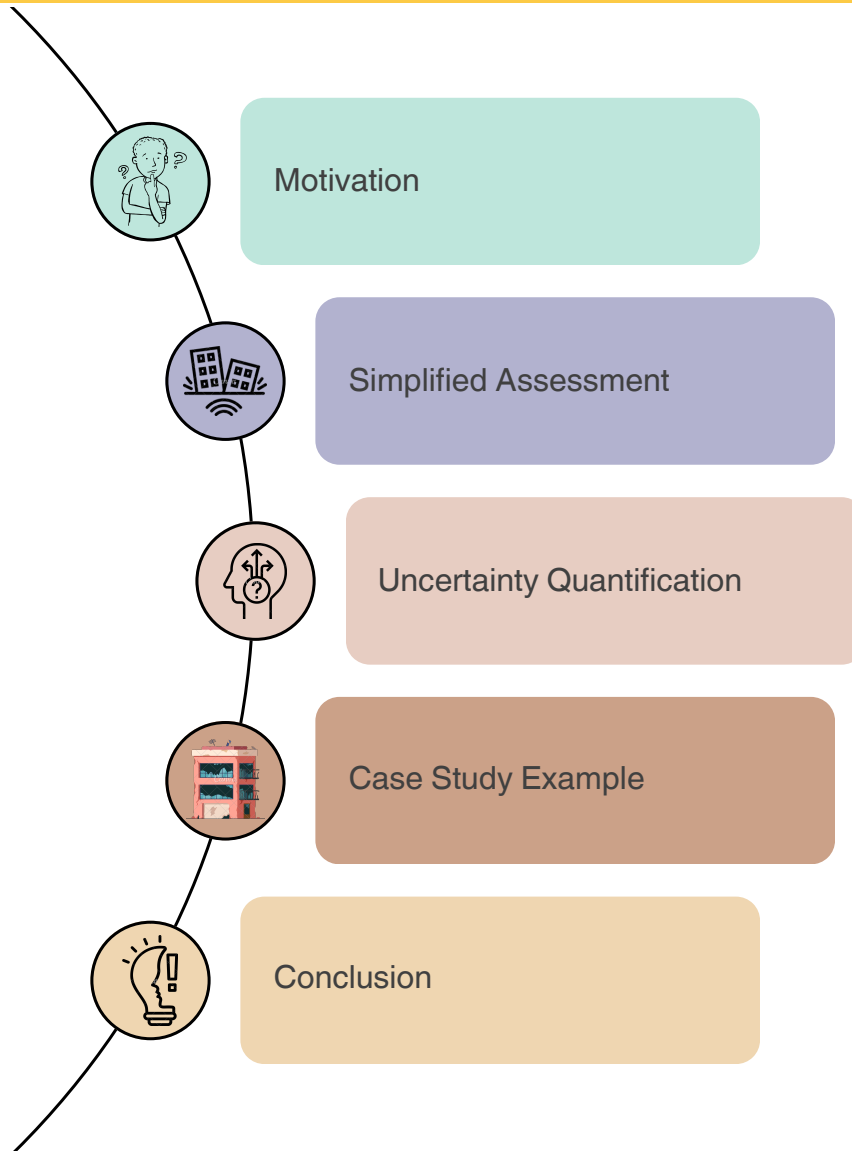
IUSS

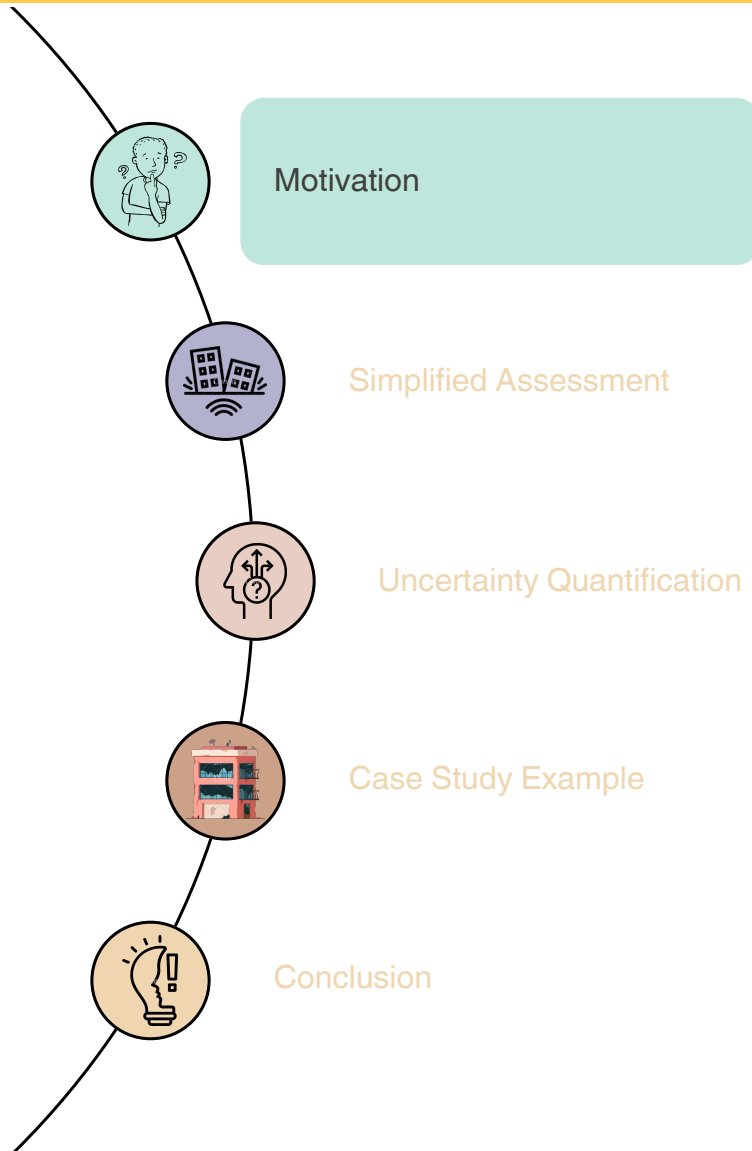
Scuola Universitaria Superiore Pavia

ROSE Centre

Centre for Training and Research
on Reduction of Seismic Risk

Web: www.iusspavia.it/rose Email: rose@iusspavia.it







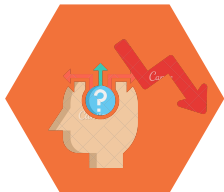
Statistical Significance in Regional Building Stocks



High Vulnerability to Ground-Shaking Events



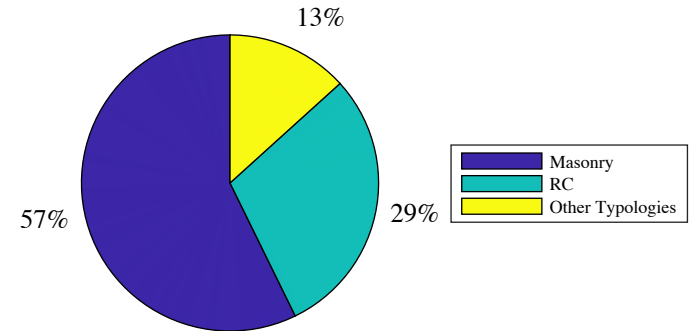
Accurate Response Characterisation



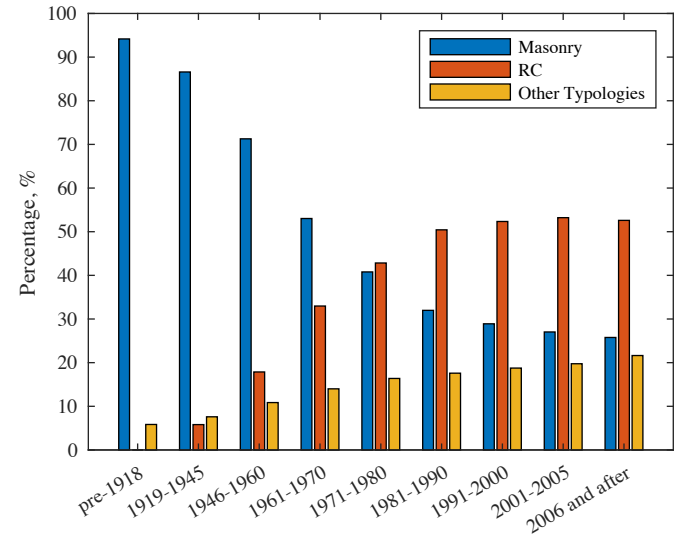
Reduction of Uncertainty in Risk and Loss-Based Applications



Improved Decision-Making and Overall Community Resilience



Residential buildings by construction material



*Residential buildings by period of construction
and construction material*



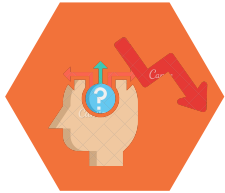
**Statistical Significance in
Regional Building Stocks**



**High Vulnerability to Ground-
Shaking Events**



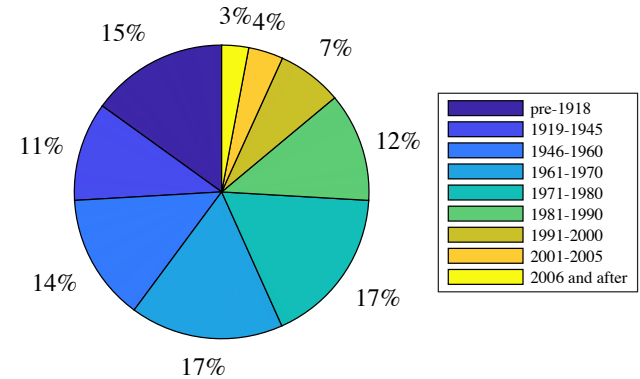
**Accurate Response
Characterisation**



**Reduction of Uncertainty in Risk-
and Loss-Based Applications**



**Improved Decision-Making and
Overall Community Resilience**



Residential buildings by period of construction



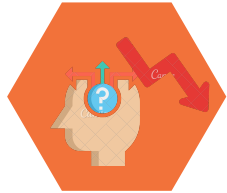
**Statistical Significance in
Regional Building Stocks**



**High Vulnerability to Ground-
Shaking Events**



**Accurate Response
Characterisation**



**Reduction of Uncertainty in Risk-
and Loss-Based Applications**



**Improved Decision-Making and
Overall Community Resilience**



Damage observations following earthquake events



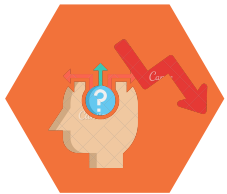
**Statistical Significance in
Regional Building Stocks**



**High Vulnerability to Ground-
Shaking Events**



**Accurate Response
Characterisation**



**Reduction of Uncertainty in Risk-
and Loss-Based Applications**

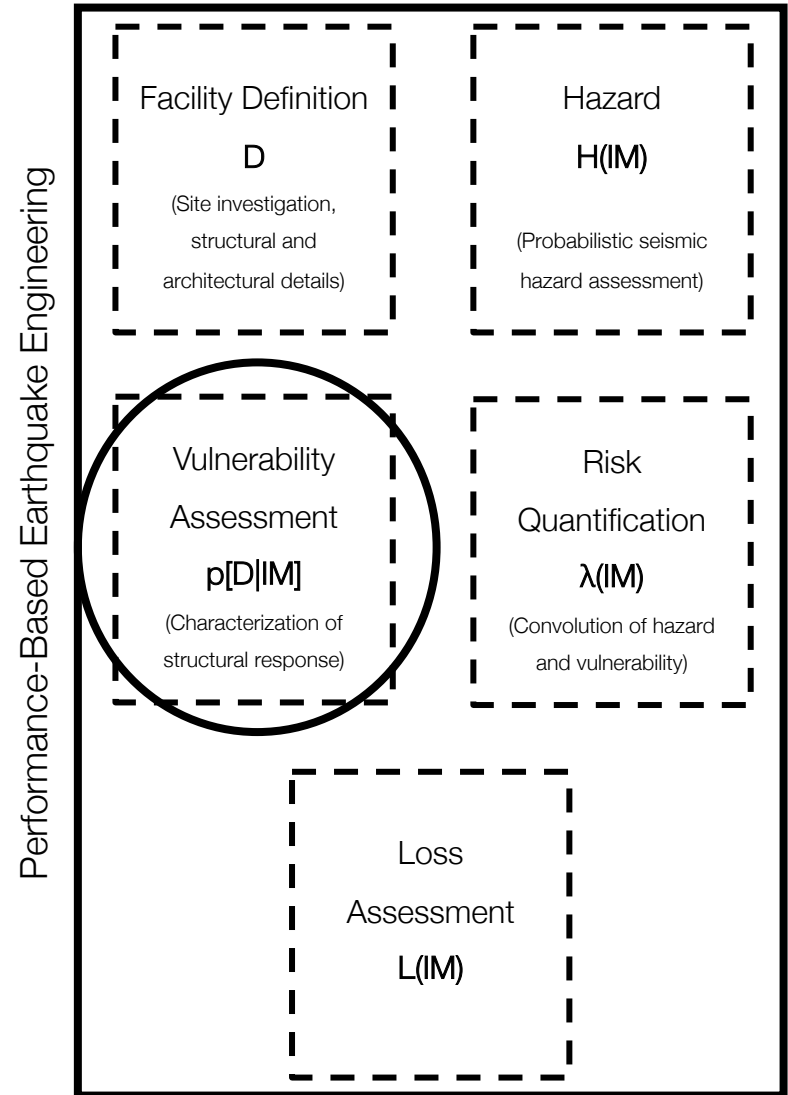


**Improved Decision-Making and
Overall Community Resilience**



Predicted \approx Observed

Analytical \gg Empirical





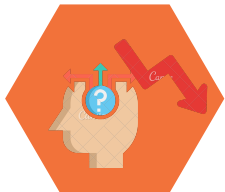
**Statistical Significance in
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**Accurate Response
Characterisation**



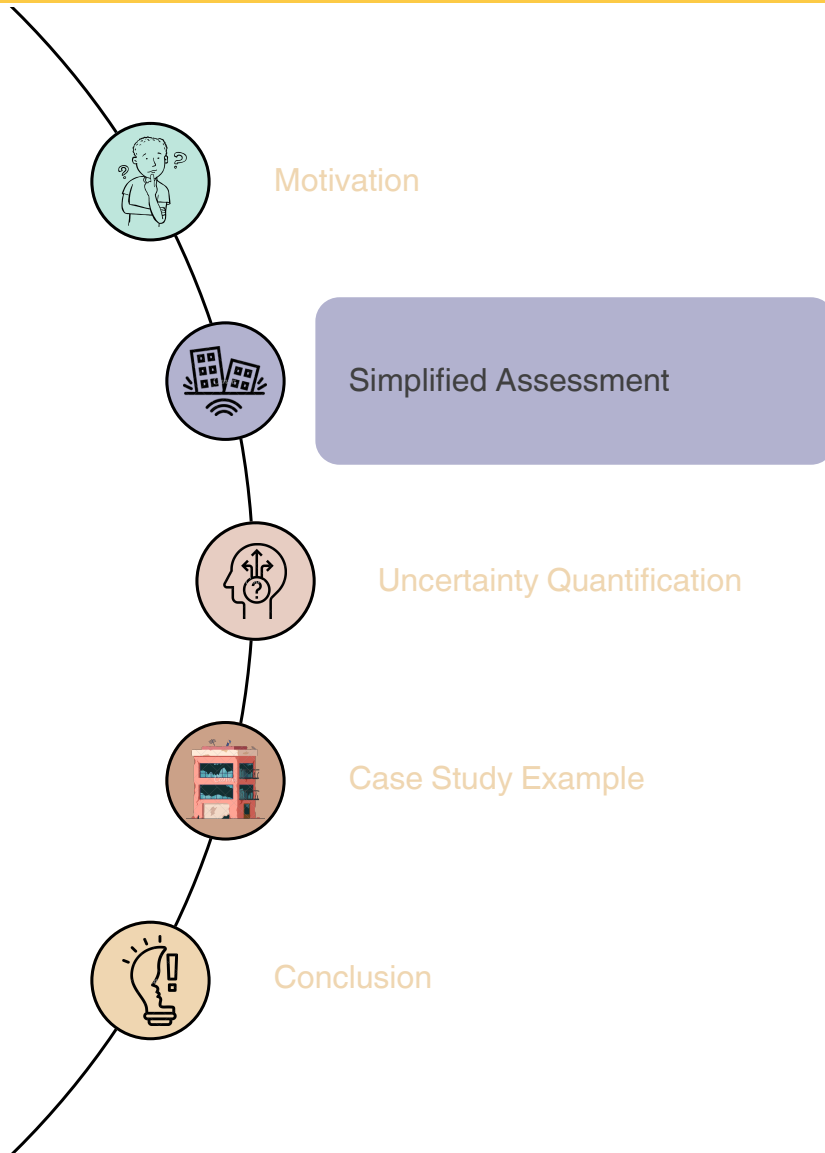
**Reduction of Uncertainty in Risk-
and Loss-Based Applications**

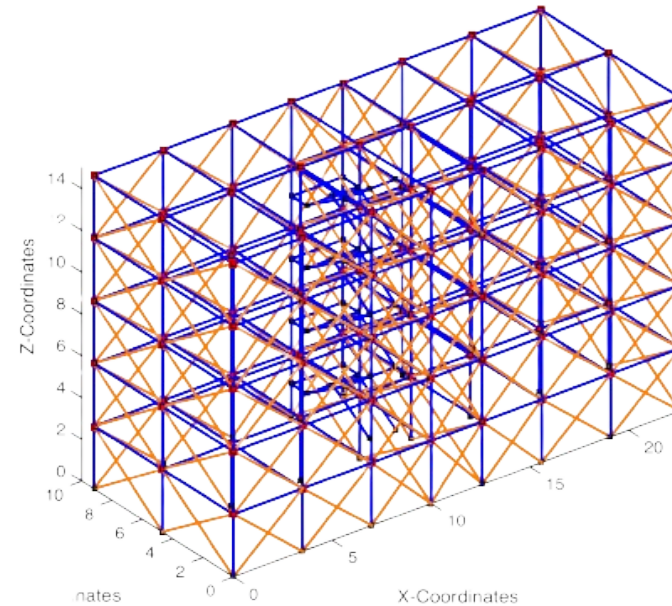
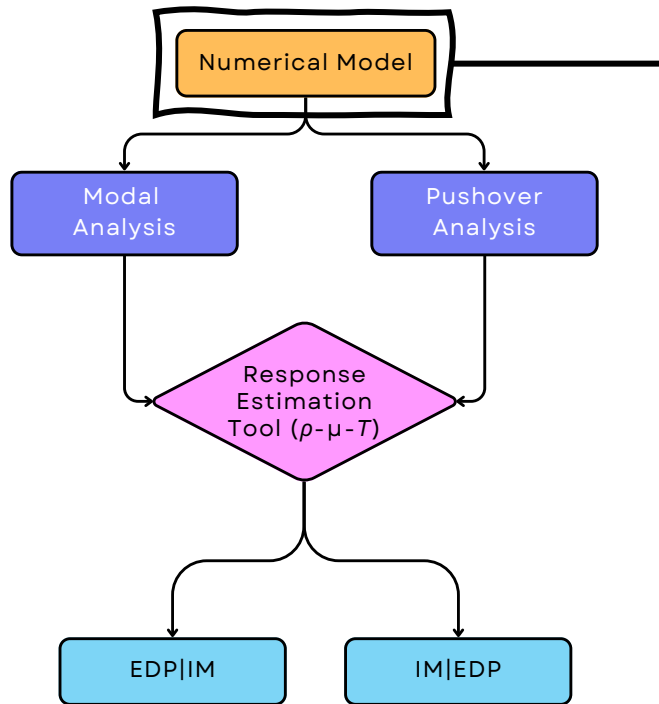


**Improved Decision-Making and
Overall Community Resilience**

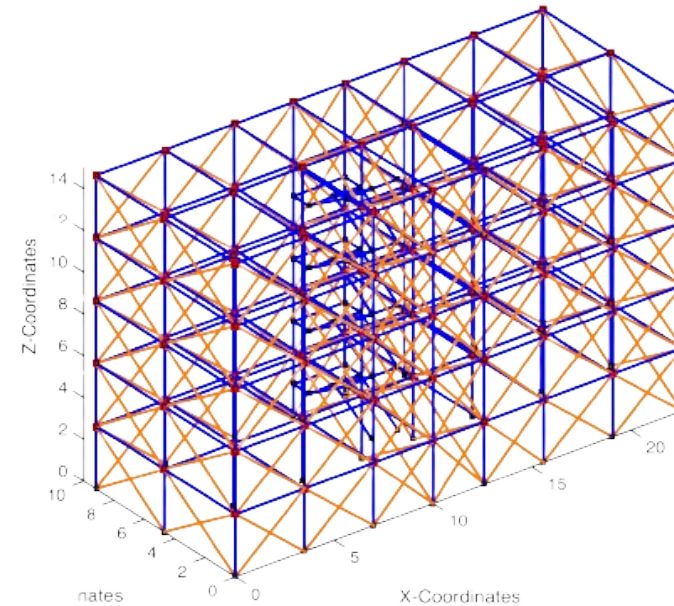
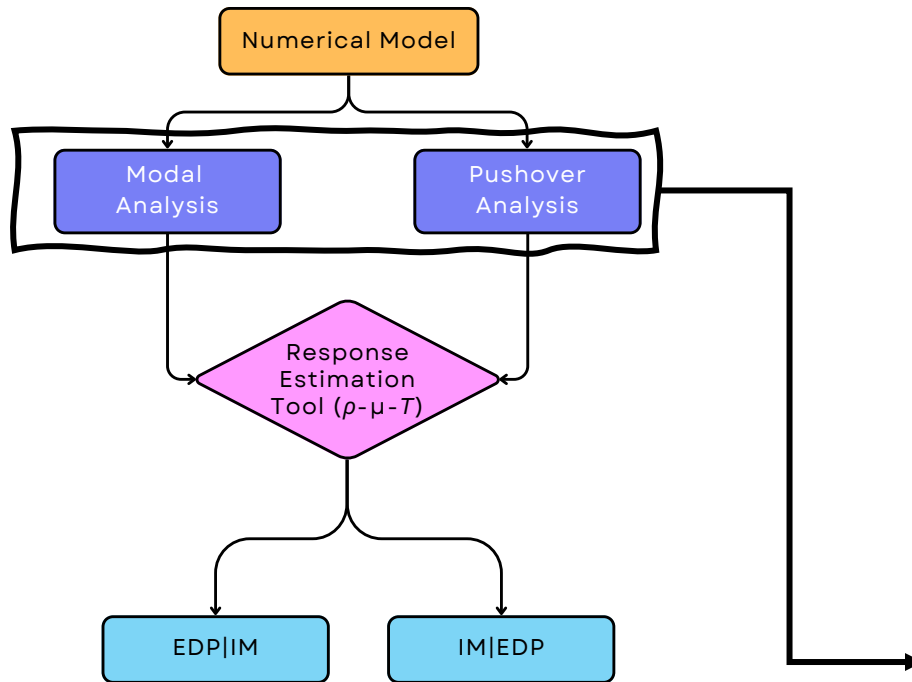


- *Adequate characterization of structural response*
- *Reduction and mitigation of seismic risk*
- *Drafting prioritization schemes and policies*
- *Retrofitting and structural rehabilitation*
- *Adequate allocation of resources*
- *Minimization of direct and indirect seismic losses*

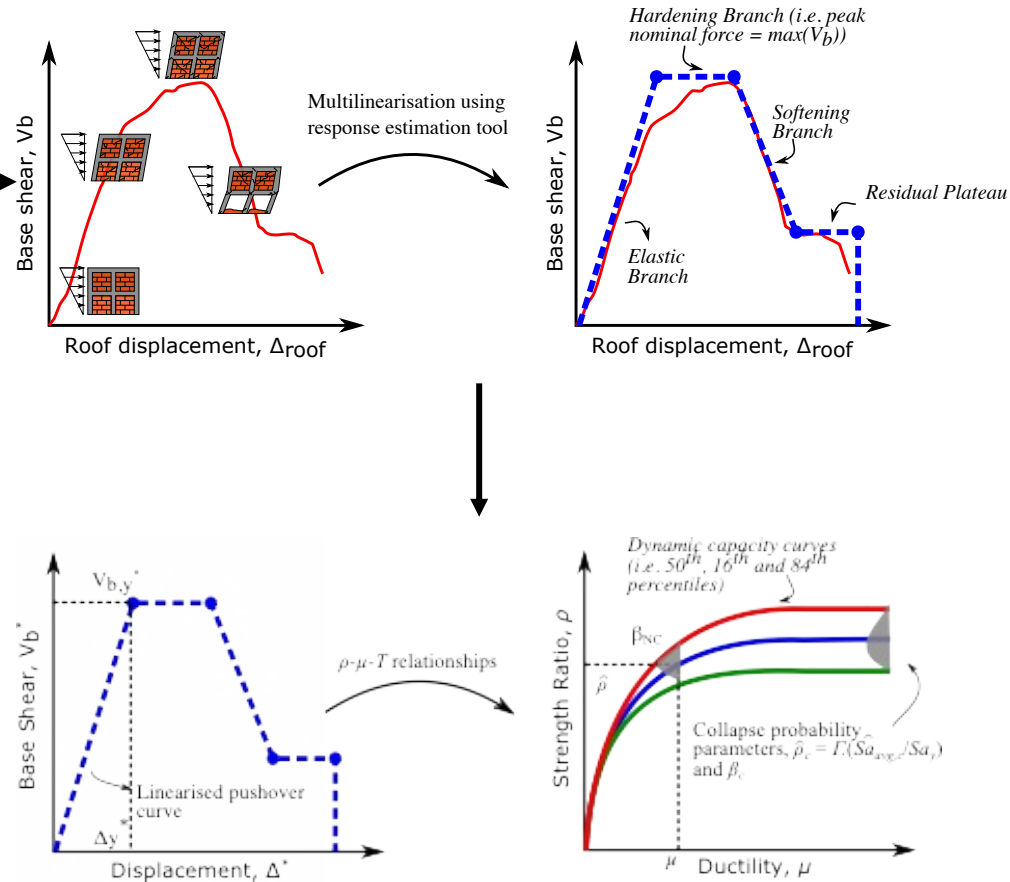
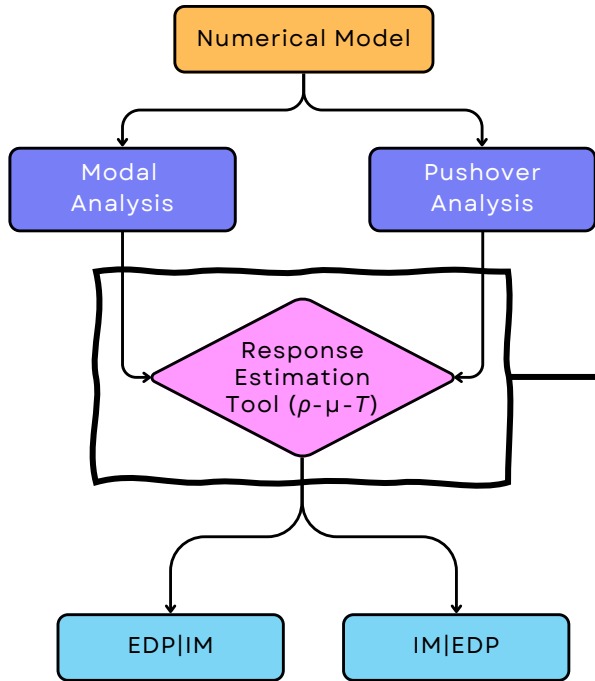


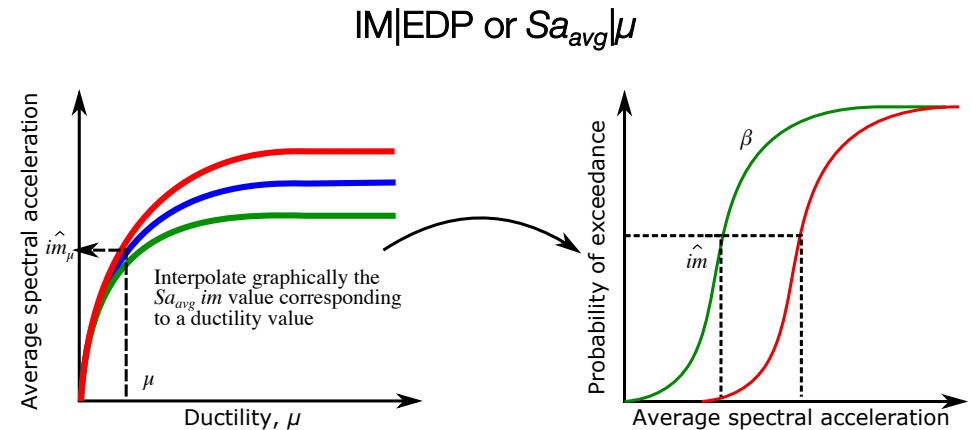
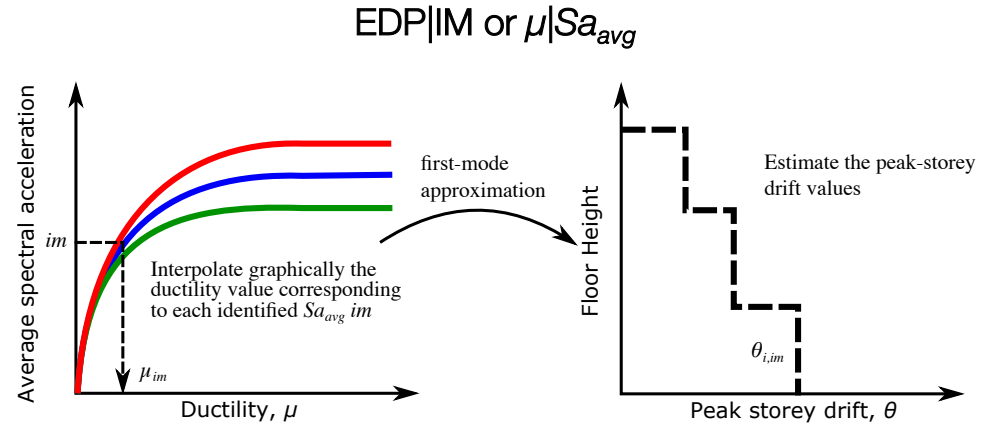
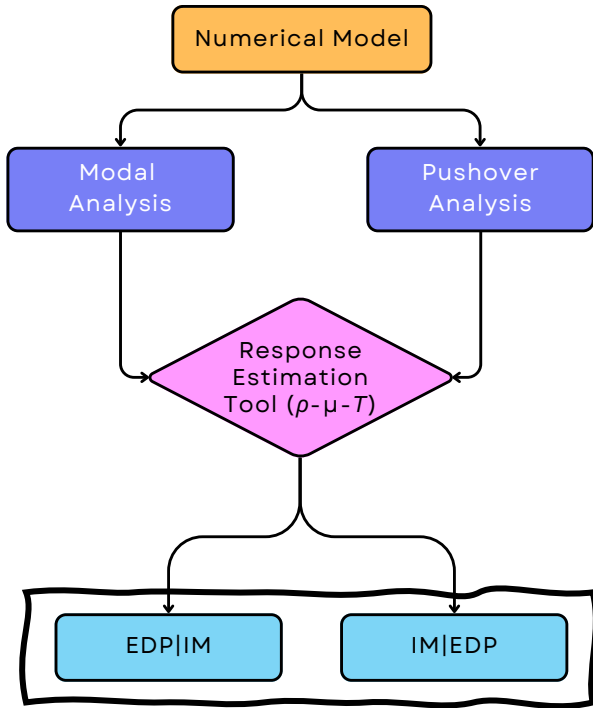


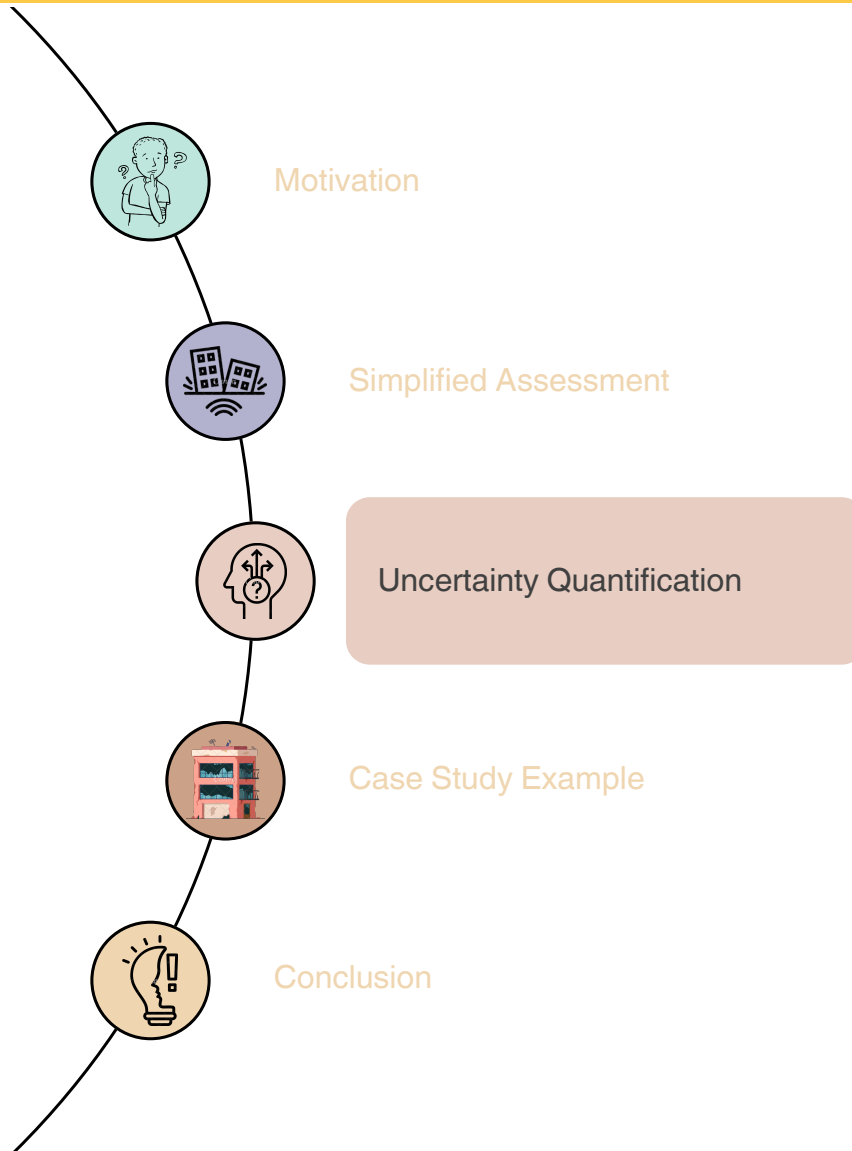
- Detailed numerical model;
- Must account for all possible inelastic mechanisms and failure modes;



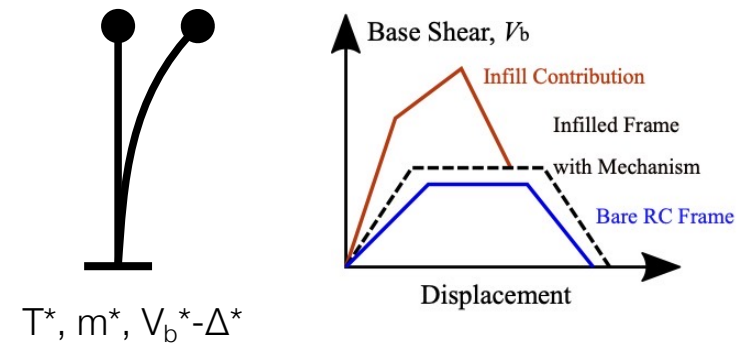
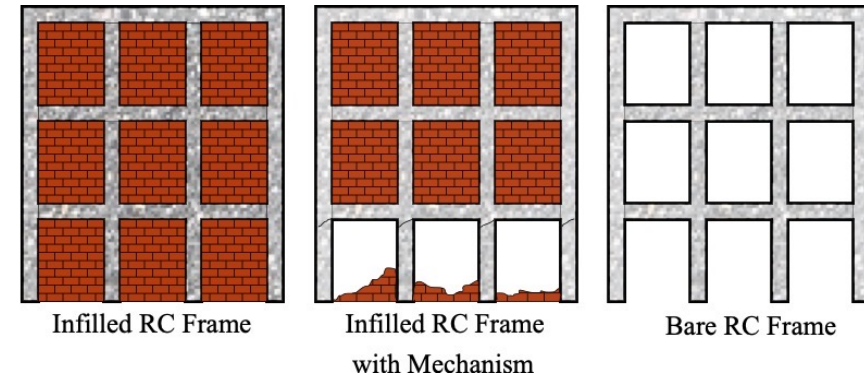
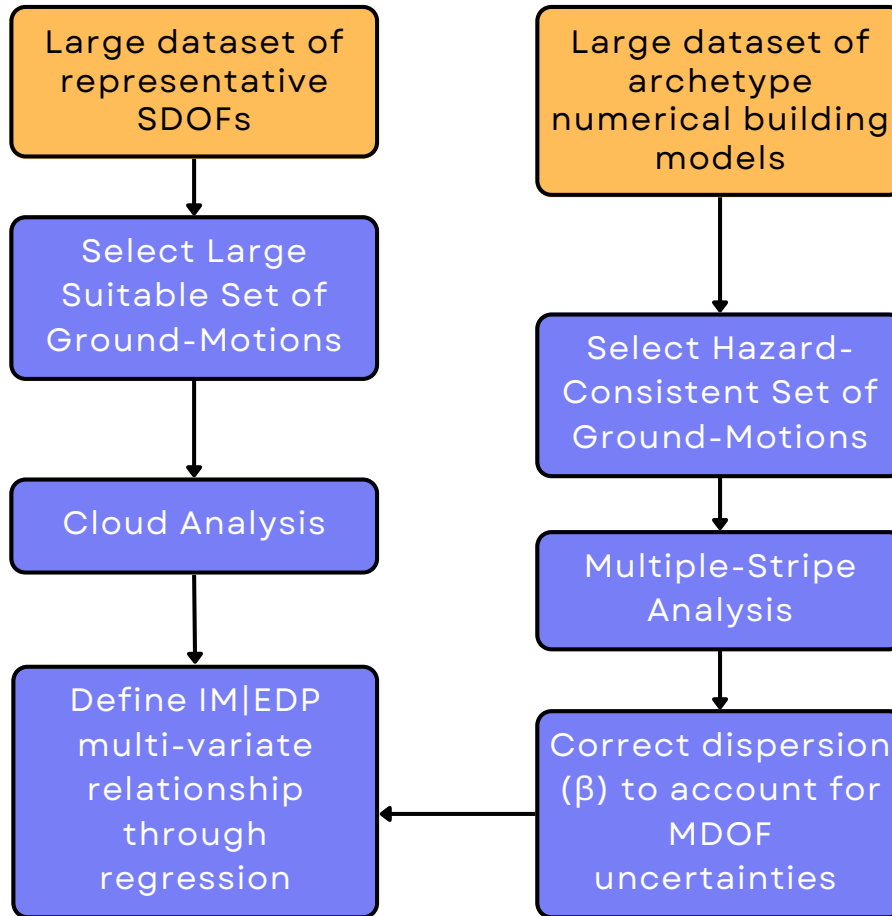
- Perform eigenvalue analysis to extract first-mode shape ordinates;
- Perform nonlinear static pushover to characterize the lateral response of the MDOF system (i.e., base-shear vs roof displacement);





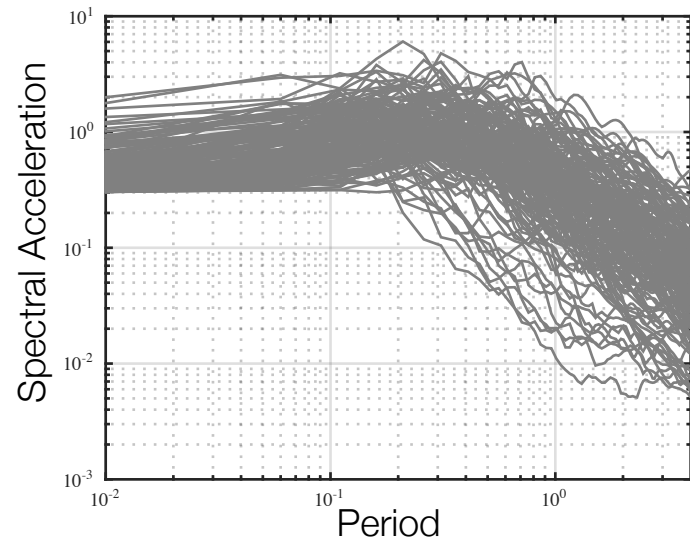
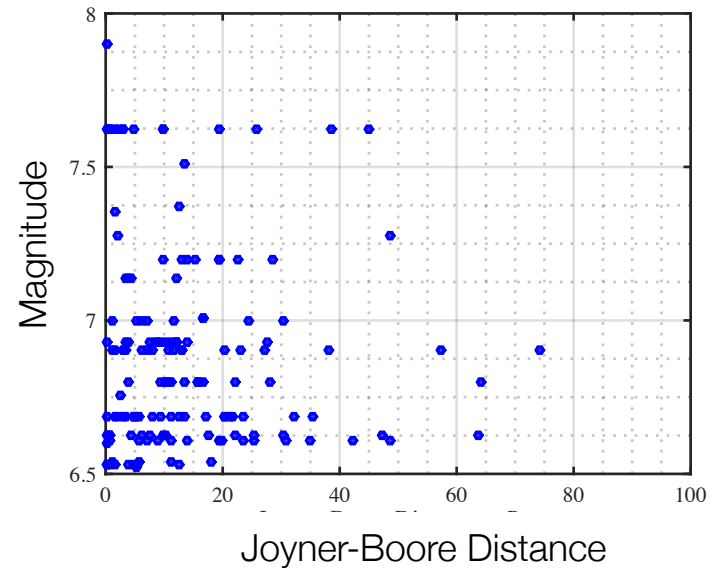
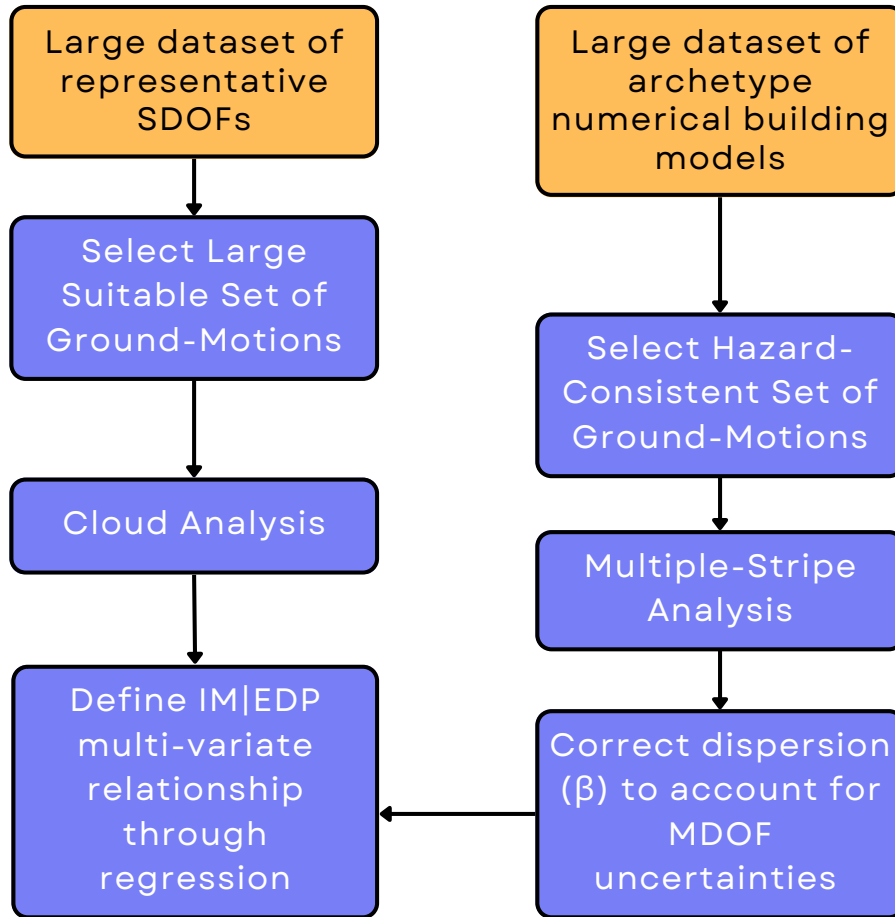


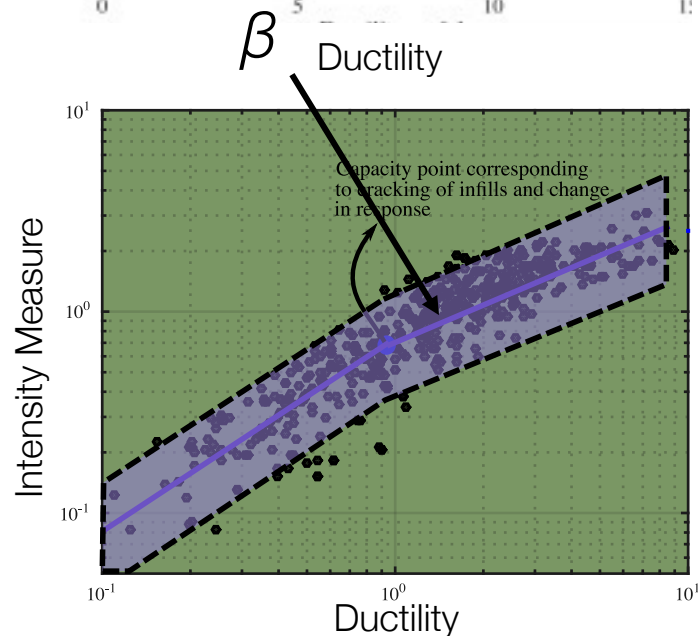
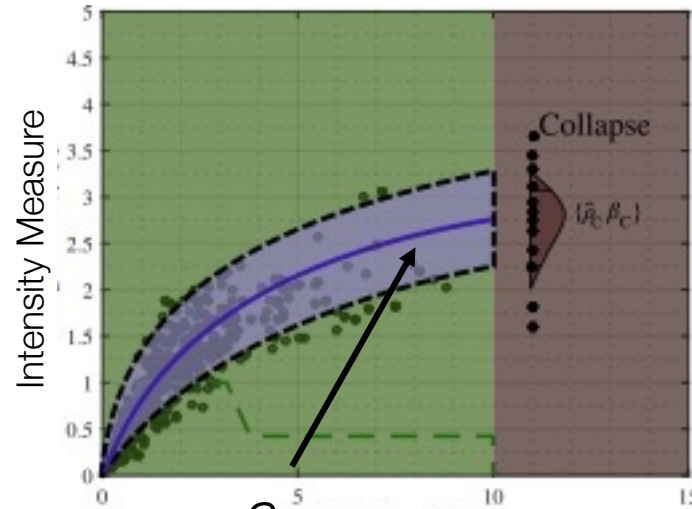
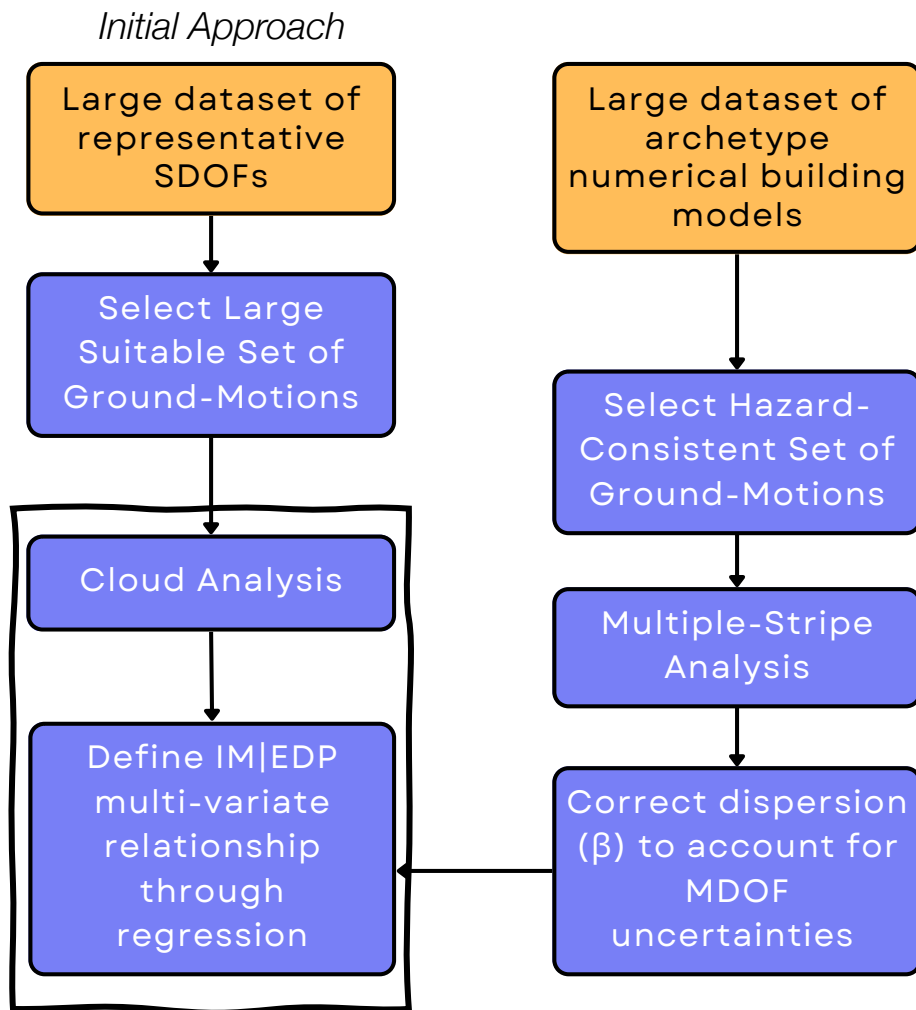
Initial Approach



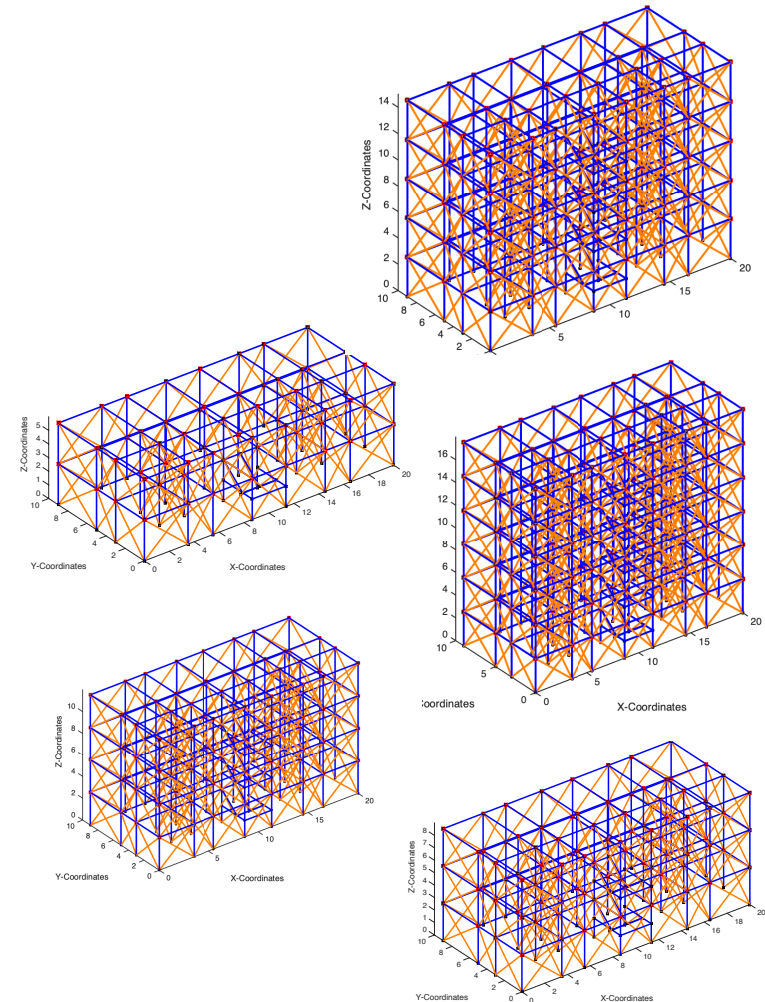
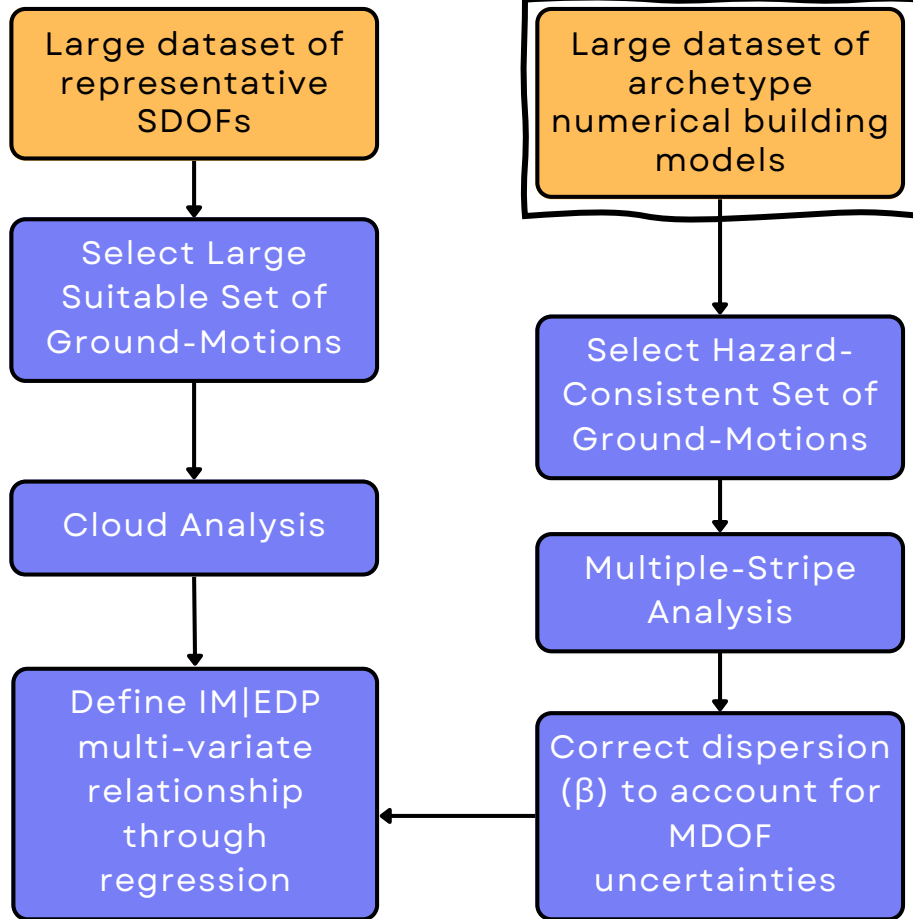
Equivalent SDOF Definition

Initial Approach



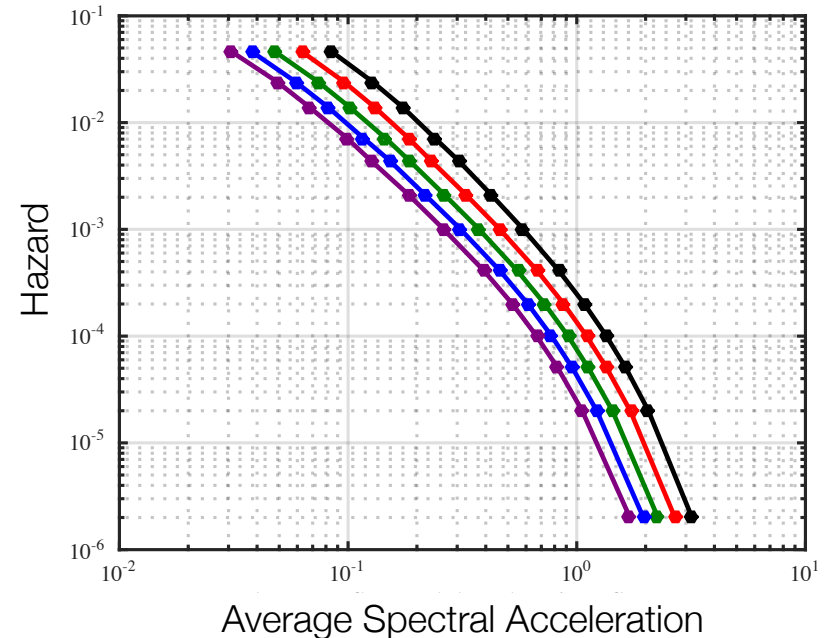
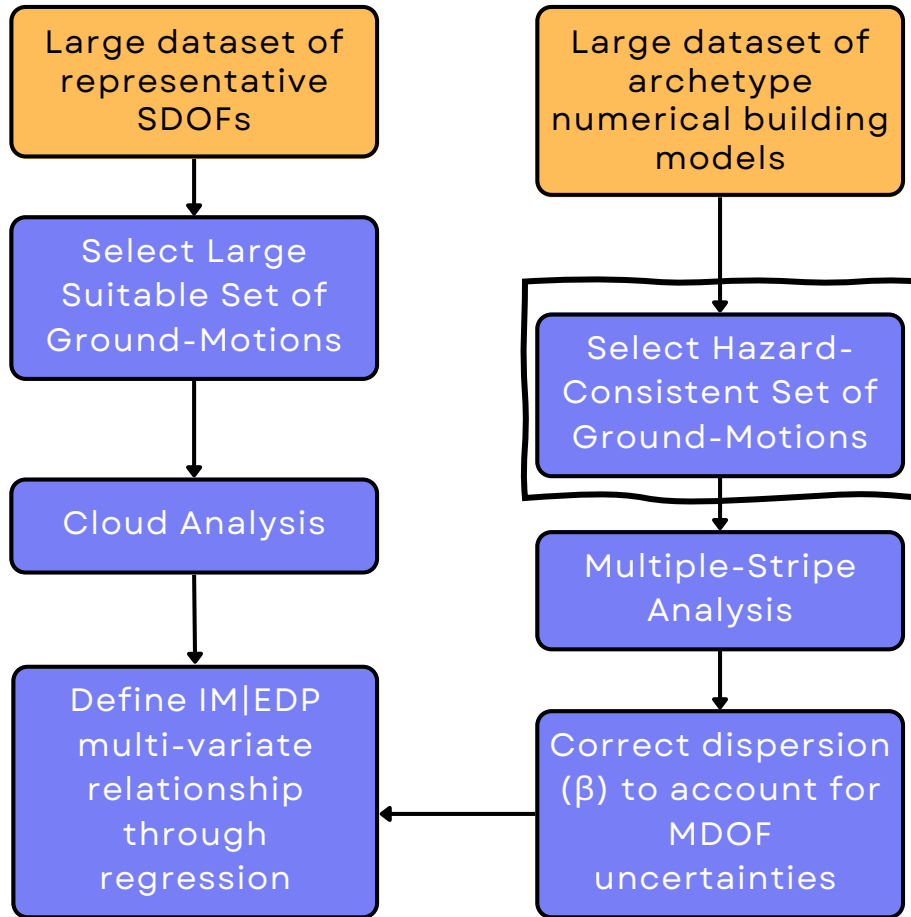


Correction



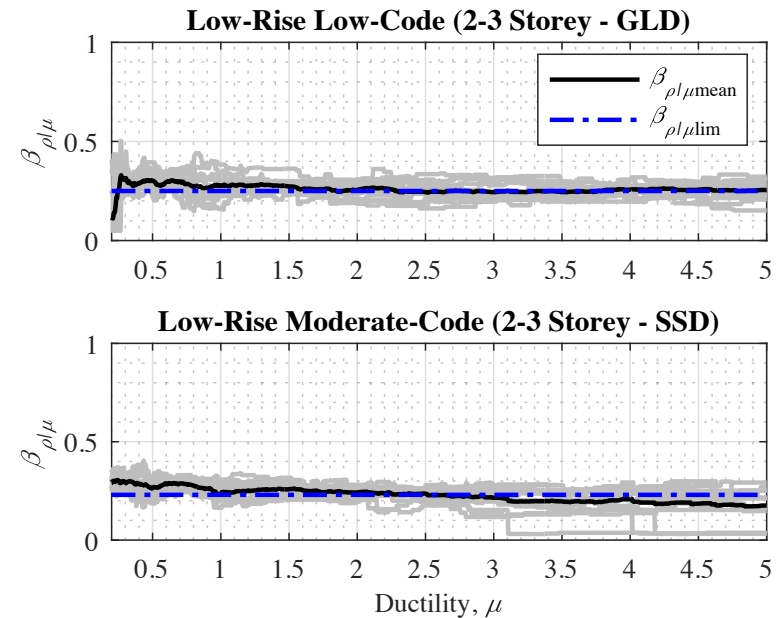
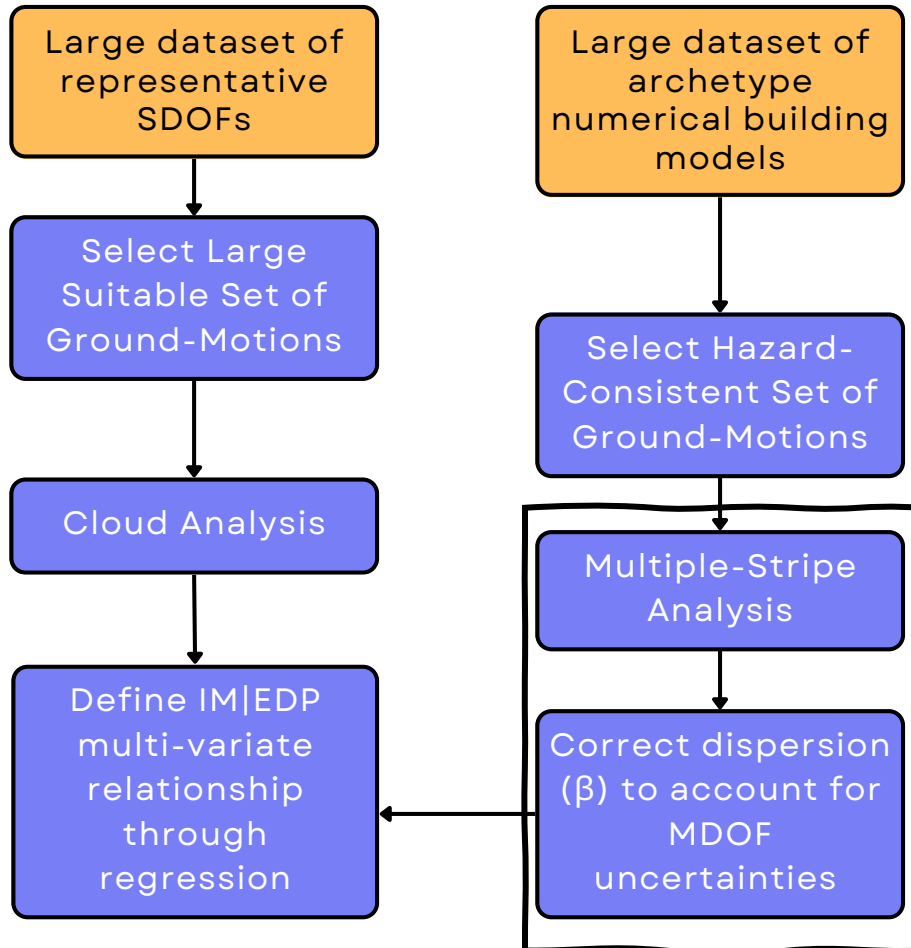
Total 105 low-rise and mid-rise infilled RC building archetypes

Correction

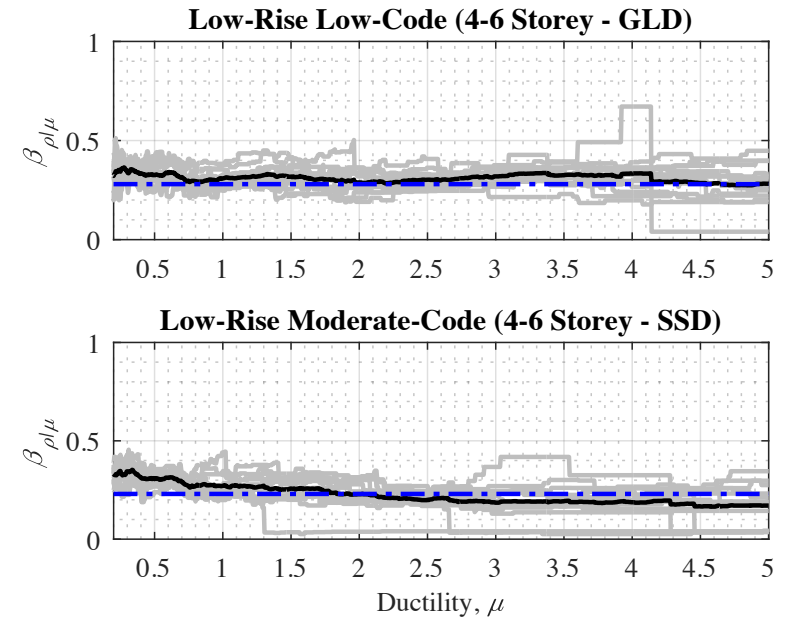
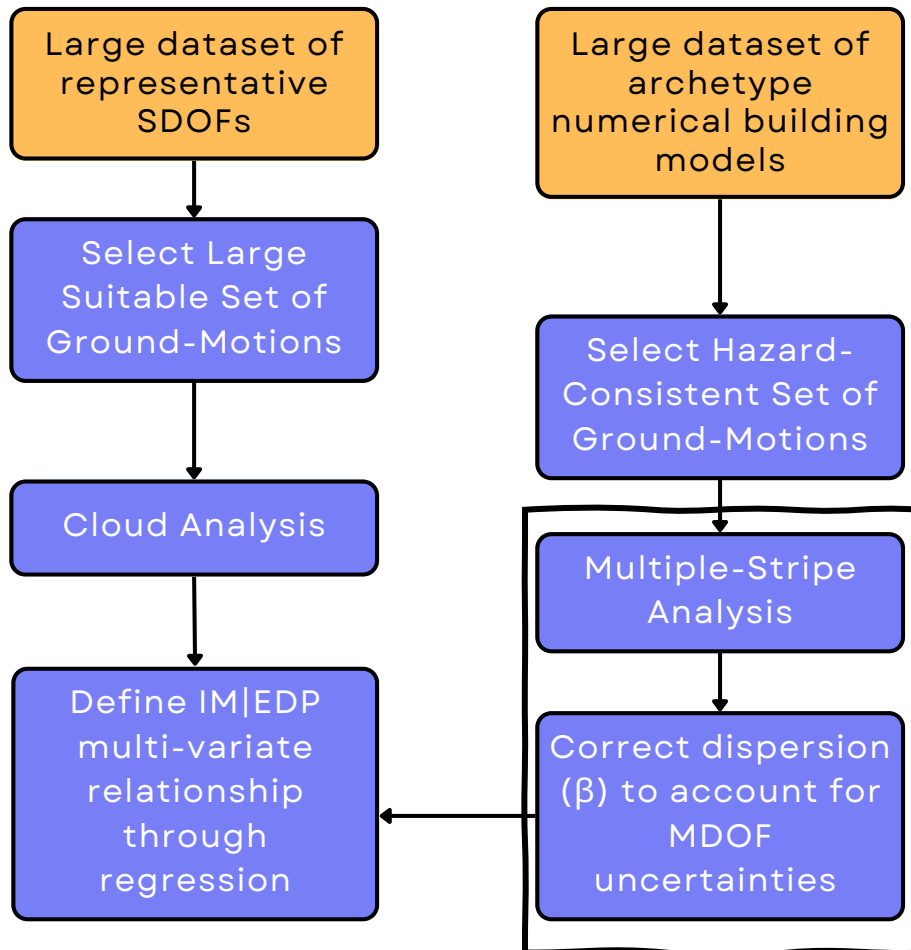


Probabilistic seismic hazard assessment expressing the hazard in L'Aquila, Italy in terms of the average spectral acceleration corresponding to conditioning periods of $T^=0.2-0.6s$*

Correction

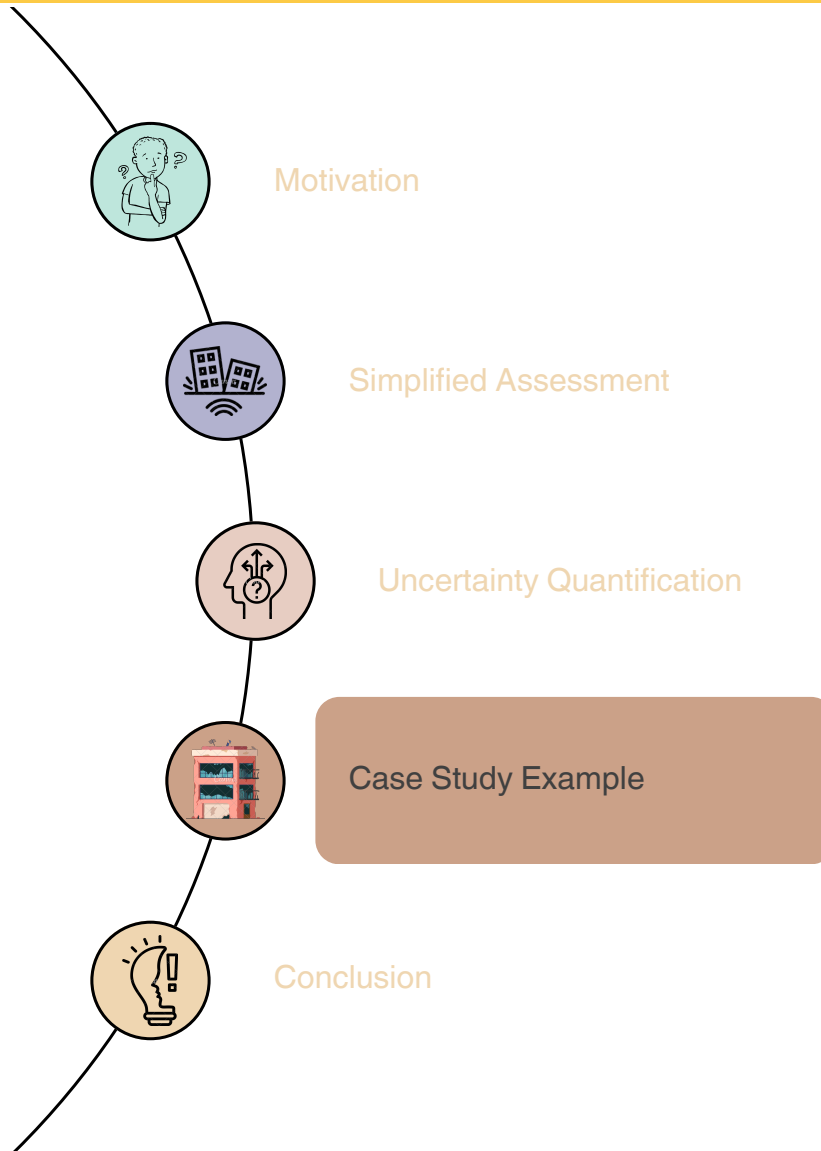


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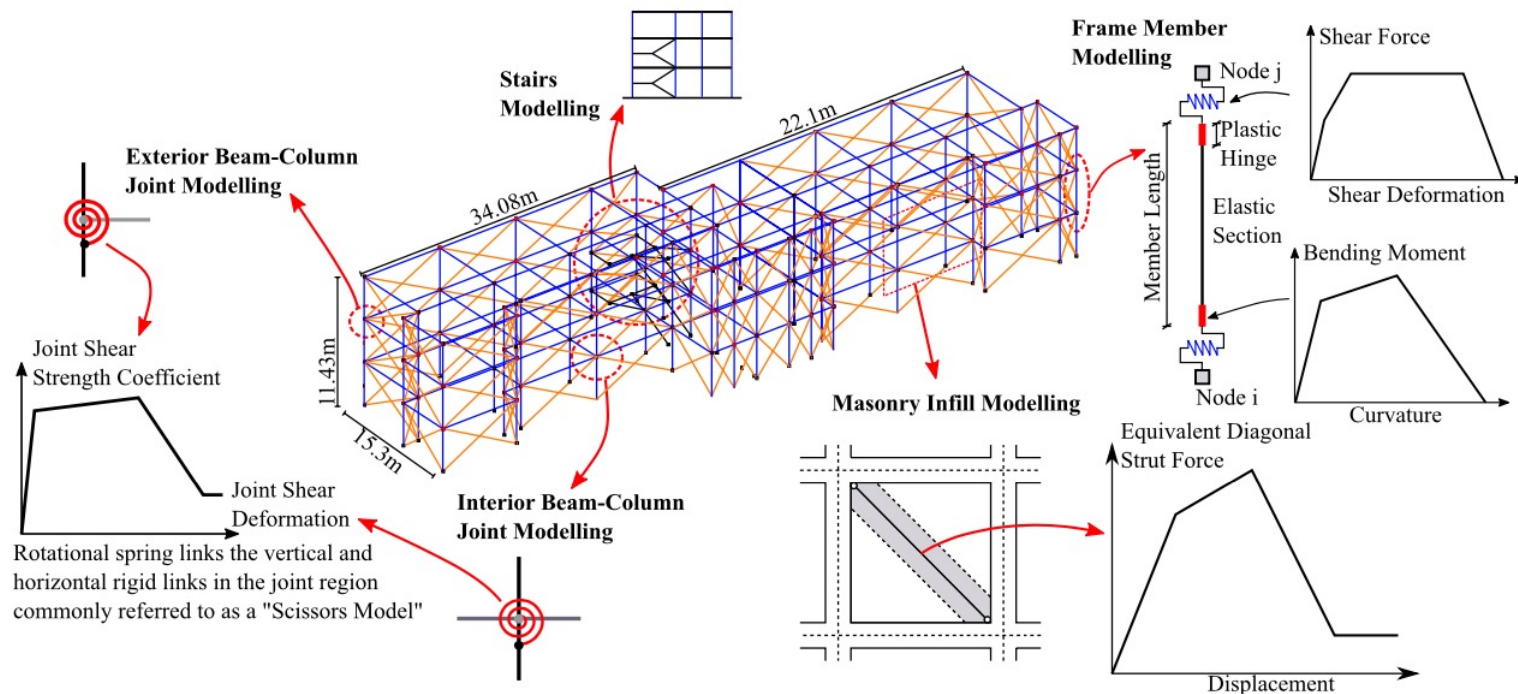


*Suggested value of IM|EDP uncertainty for low and mid-rise infilled RC
buildings*

Seismic Code Level	Number of Stories	Taxonomy Code	Suggested Dispersion, β
Low (GLD)	Low-rise (2-3)	LC-LR	0.25
	Mid-rise (4-6)	LC-MR	0.23
Moderate (SSD)	Low-rise (2-3)	MC-LR	0.28
	Mid-rise (4-6)	MC-MR	0.23



- Three-storey RC school building with masonry infills;
- Located in Napoli, Italy;
- Constructed in the 1960s, before the introduction of modern seismic design guidelines;

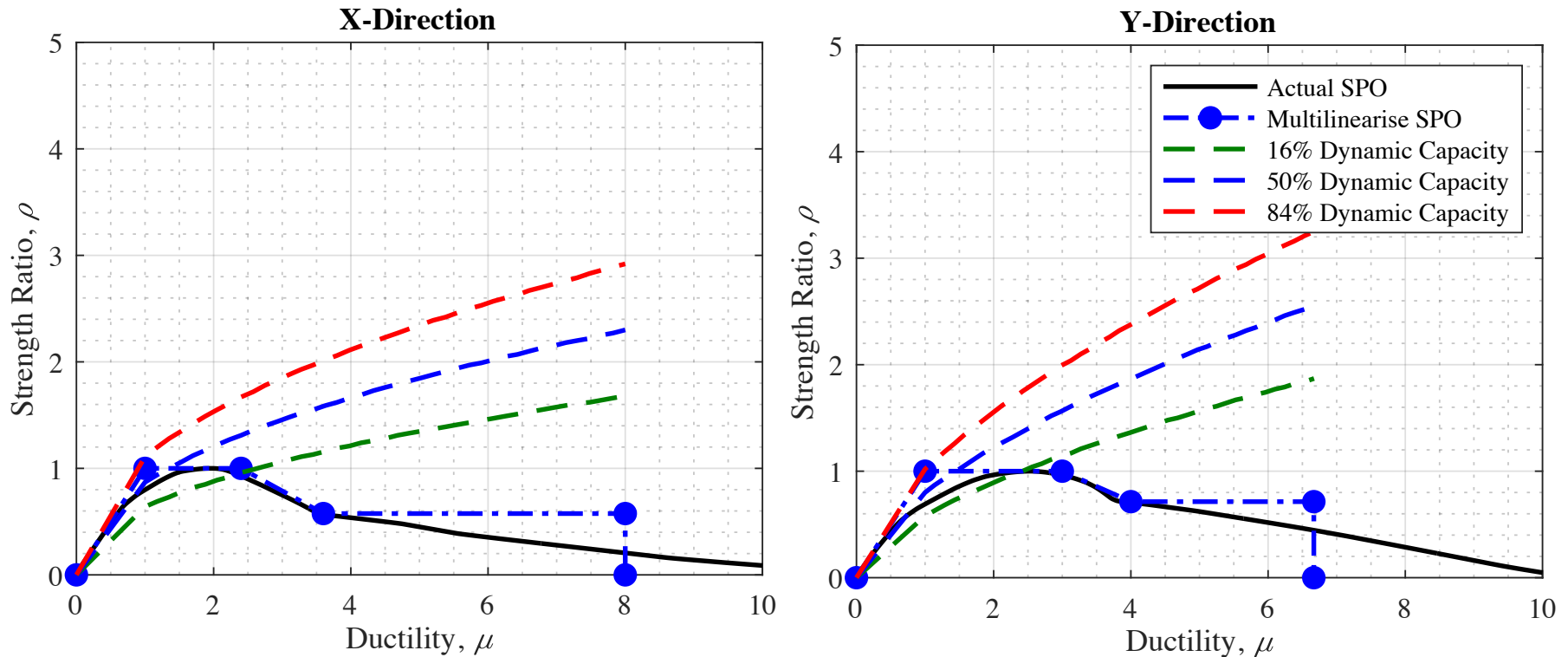


General layout and numerical modelling techniques of the case study school building.

Summary of the modal properties of the case study building in both principal directions

Floor No.	Mass, m_i [tonnes]	X-Direction			Y-Direction (Weaker Direction)		
		First-mode shape, ϕ	Period, T_1 [s]	Yield spectral acceleration, S_{a_y} [g]	First-mode shape, ϕ	Period, T_1 [s]	Yield spectral acceleration, S_{a_y} [g]
Base	0	0.00	0.62	0.42	0.00	0.36	0.40
First	985	0.22			0.22		
Second	960	0.56			0.57		
Third	806	1.00			1.00		

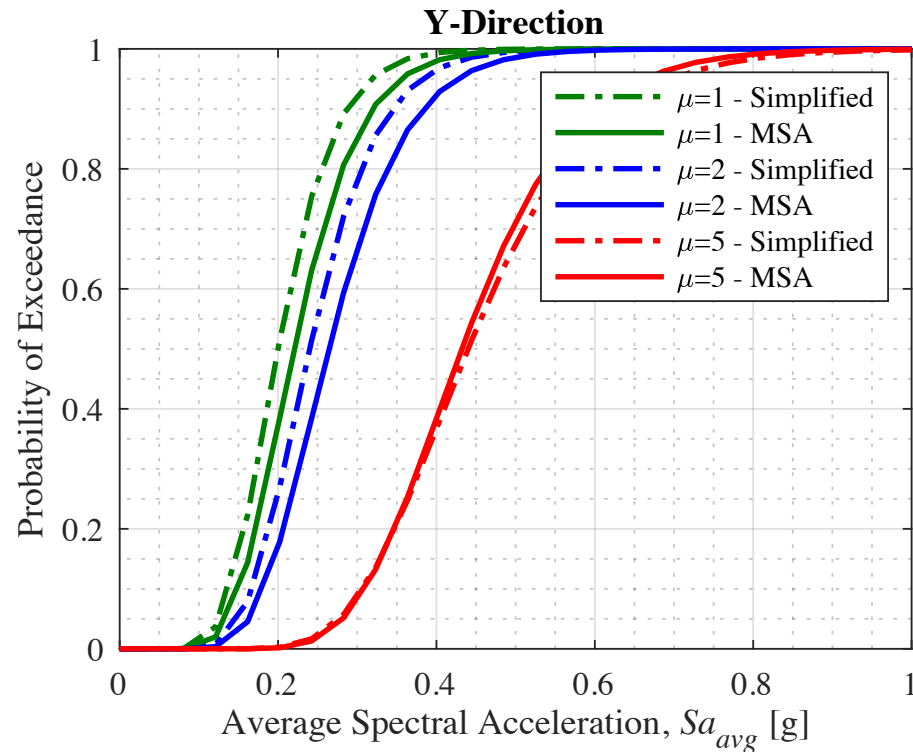
Summary of the static pushover analyses of the case study building in both principal directions



Summary of the fragility function comparisons

Ductility Thresholds	Simplified Assessment		Extensive Assessment (MSA)	
	Median intensity, $S_{a_{avg}}$ [g]	Dispersion, β	Median intensity, $S_{a_{avg}}$ [g]	Dispersion, β
$\mu=1$	0.20	0.25	0.22	0.28
$\mu=2$	0.24		0.27	0.26
$\mu=5$	0.44		0.43	0.26

Summary of the fragility function comparisons



Seismic Risk Calculation:

- Classical Approach:

$$\lambda = \int_0^{+\infty} P[\mu \geq \mu | IM = s] |dH(s)|$$

- Pushover-Based Risk Estimation (PB-Risk):

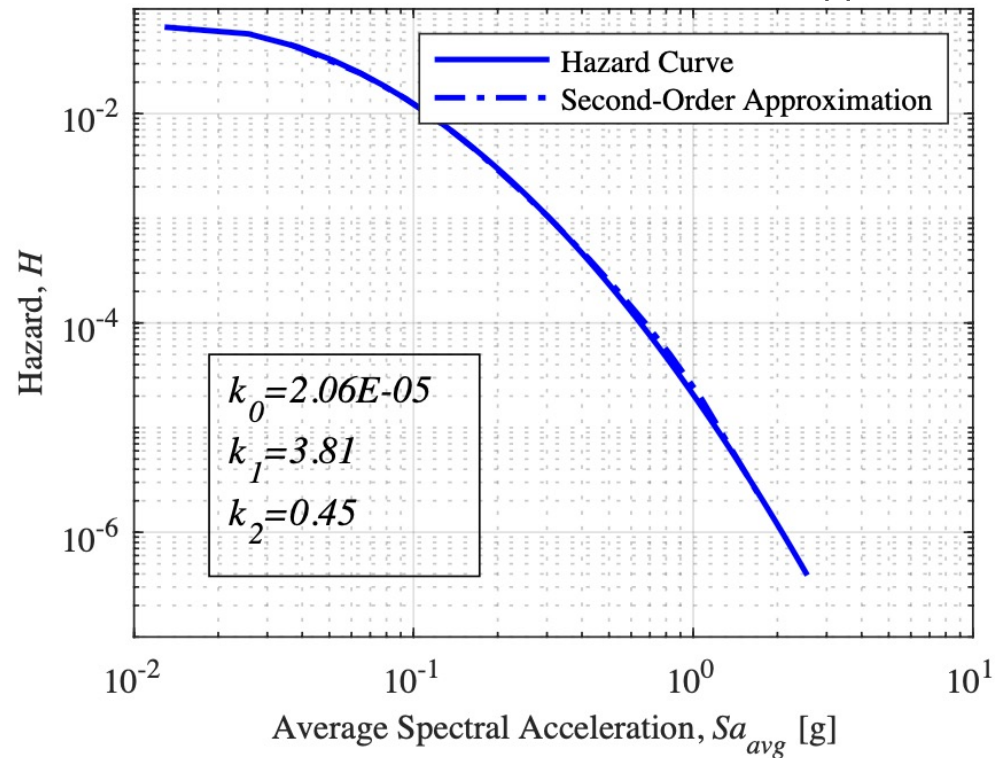
1. Second-order approximation of the hazard function:

$$H(s) = k_0 \exp [-k_2 \ln^2(s) - k_1 \ln(s)]$$

2. Application of IM-based closed form expressions:

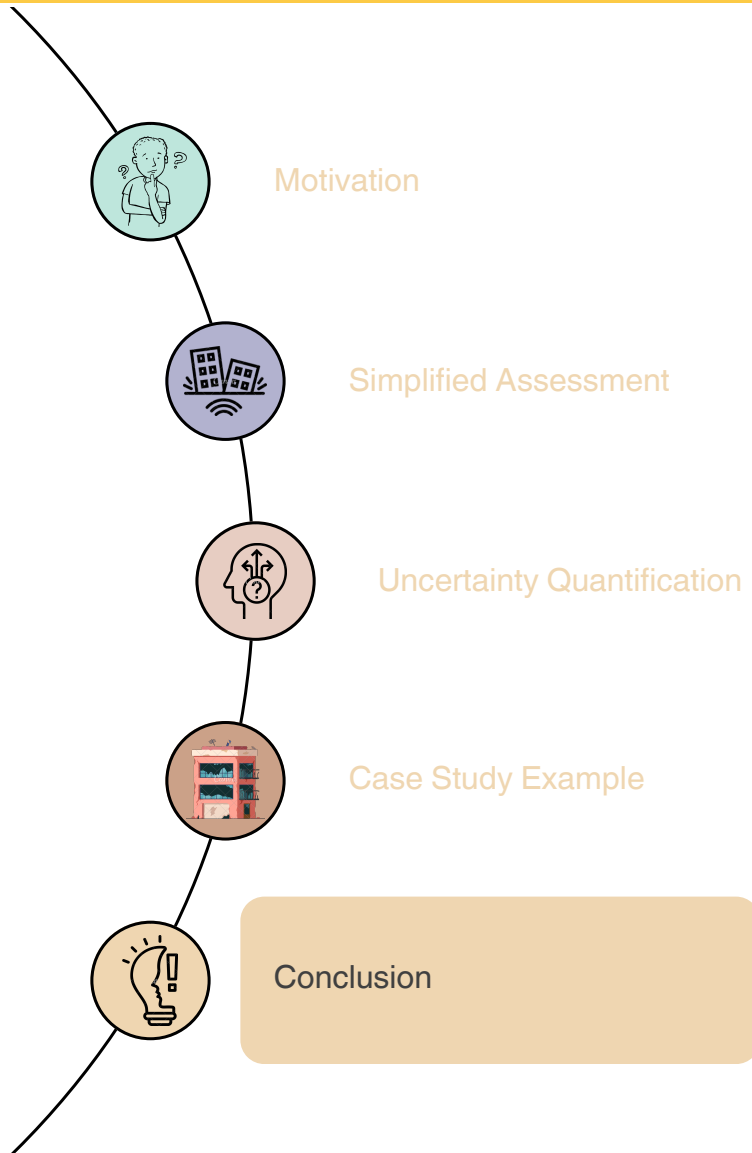
$$\lambda = \sqrt{p} k_0^{1-p} [H(s)]^p \exp \left[\frac{k_1^2}{4k_2} (1-p) \right]$$
$$p = \frac{1}{1 + 2k_2\beta^2}$$

Seismic hazard characterization and second-order approximation



Summary of the risk assessment comparisons

Ductility Thresholds	PB-Risk	Classical	Error in MAFE estimation
	Mean annual frequency of exceedance (MAFE), λ		
$\mu=1$	0.0031	0.0029	6.89%
$\mu=2$	0.0021	0.0019	10.52%
$\mu=5$	4.92E-04	5.02E-04	1.6%



- A simplified tool for the seismic performance assessment of infilled RC frames was presented;
- The epistemic uncertainty associated with structural response (IM|EDP) was quantified for the infilled RC typology and different sub-taxonomies;
- The suggested values of the record-to-record variability could be incorporated with other simplified methodologies for the derivation of fragility functions or risk metrics (e.g. *PB-Risk*);
- The suggested values were validated on a case-study school buildings where an adequate match in terms of vulnerability and risk parameters was observed;
- Good agreement between the results of classical and simplified methodologies;

Links:

- Database of Archetype Building Models:

<https://github.com/gerardjoreilly/Infilled-RC-Building-Database>

- Response Estimation Tool for Infilled RC Frame Structures:

<https://github.com/gerardjoreilly/Infilled-RC-Building-Response-Estimation>

Publications:

- Nafeh A.M.B., O'Reilly G.J. (2022) Unbiased simplified seismic fragility estimation of non-ductile infilled RC structures. *Soil Dynamics and Earthquake Engineering* 157:107253. <https://doi.org/10.1016/j.soildyn.2022.107253>
- *PB-Risk*: Nafeh, A.M.B., O'Reilly, G.J. (2023) Simplified pushover-based seismic risk assessment methodology for existing infilled frame structures. *Bulletin of Earthquake Engineering* 21, 2337–2368 <https://doi.org/10.1007/s10518-022-01600-y>

Thank you for your attendance
e-mail: mouayed.nafeh@iusspavia.it

